

# *The Statistical Nature of Unsteady Inlet Flow*

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# *Statistical Nature of Unsteady Inlet Flow*

*“The understanding and analysis of the unsteady information obtained from LES and DES analyses is fundamentally different from steady Reynolds Averaged Navier Stokes (RANS) analysis. That is because the process described by unsteady analyses is fundamentally stochastic in nature and not deterministic. The basic feature of the probability theory, or more commonly the statistical approach, is the transition from the consideration of a single turbulent flow within the inlet, to the consideration of a statistical ensemble of all similar turbulent flows created by the inlet. Thus the only possible description of the turbulent flow within the inlet is a statistical description based on the study of specific statistical laws, i.e. “the theory of random fields” (1)*

*(1) Monin, A. S., and Yaglom, A. M., “Statistical Fluid Mechanics”, The MIT Press, Cambridge, Massachusetts, 1971.*

# *Statistical Nature of Unsteady Inlet Flow Stochastic Processes*

*Stationary processes are unsteady flows which are statistical stable with probabilistic properties that do not change over time, in particular varying about a fixed mean level and with constant variance.*

*Non-Stationary processes are unsteady flows which exhibit no natural mean level over time and contain both coherent and random variations in their unsteady flow field structure.*

# *Statistical Nature of Unsteady Inlet Flow Homogeneous Random Processes<sup>(1)</sup>*

*“Many time series actually encountered in aerodynamics exhibit non-stationary behavior and in particular do not vary about a fixed mean. Such series nevertheless exhibit homogeneous behavior over time of a kind. In particular, although the general level about which fluctuations are occurring may be different at different times, the broad behavior of the series, when differences in level are accounted for, may be similar over time. This behavior may be modeled in terms of an **autocorrelation operator**.”<sup>(2)</sup>*

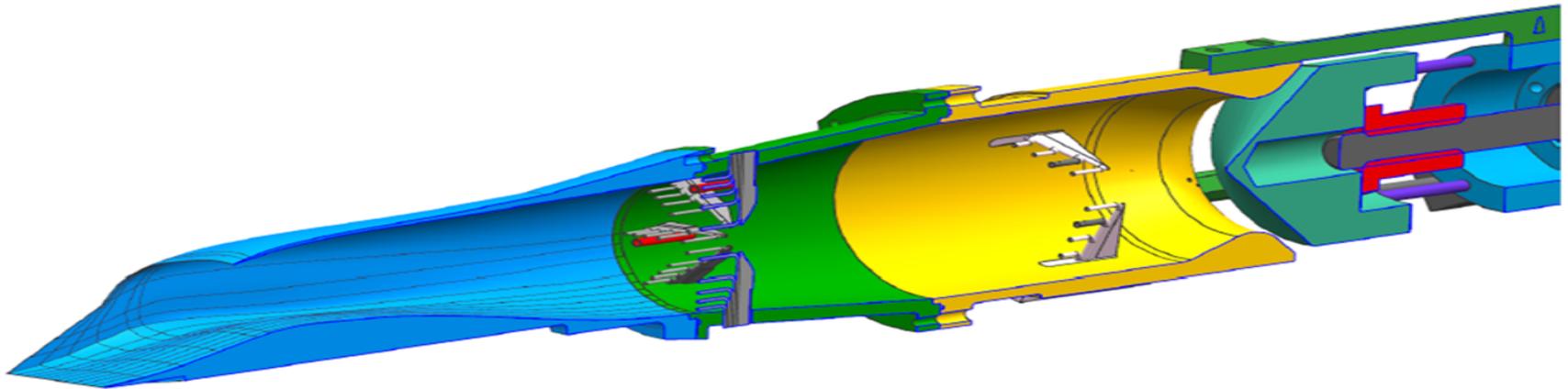
*(1) To detect coherent structures in data containing random variations.*

*(2) To identify an appropriate time series model for the mean if the data is non-stationary.*

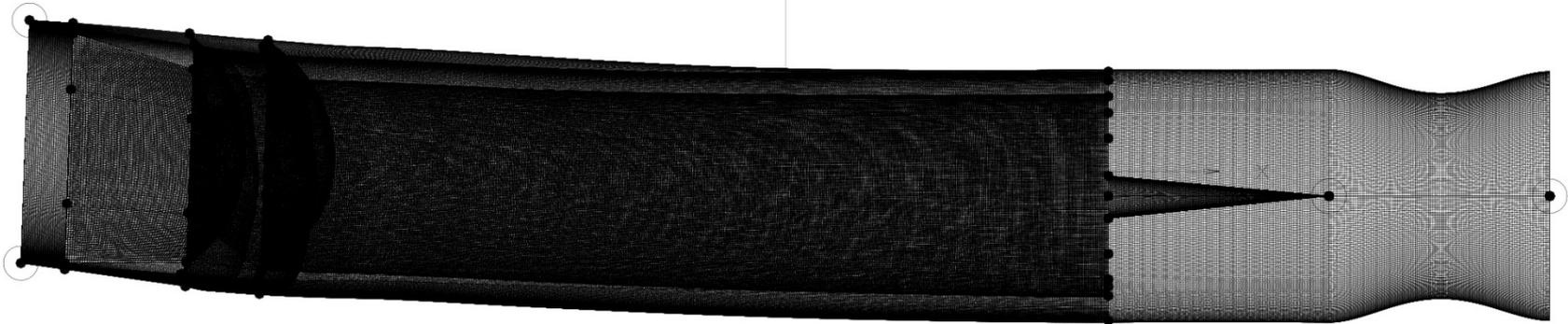
(1) George, W. K.: “Lectures in Turbulence for the 21st Century”, January, 2013

(2) Box, E. P., Jenkins, G. M., and Reinsel, G. C.: “Time Series Analysis”, John Wiley & Sons, 2008.

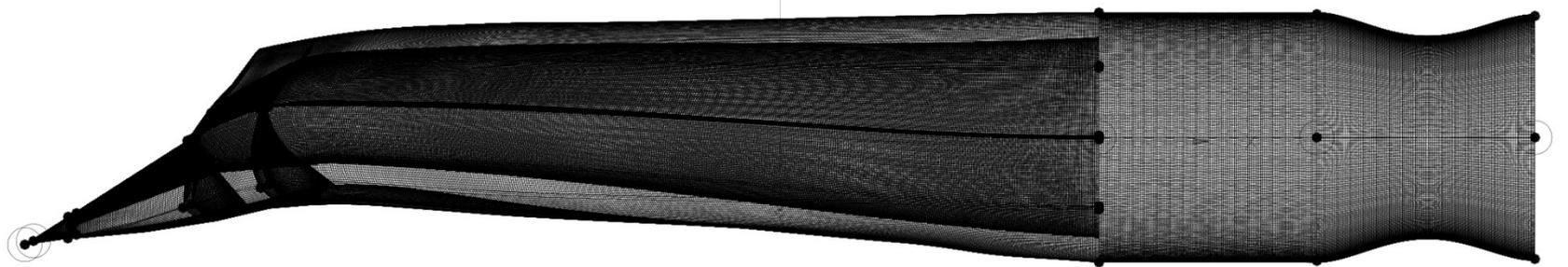
*Boeing QEVC Low Boom Supersonic Inlet Design  
8x6 NASA/GRC SWT*



*Boeing QEVC Low Boom Supersonic Inlet Design*  
*Computational Grid =  $32.945 \times 10^6$*   
*Number of Blocks = 151*



*Top View*



*Side View*

# *Boeing QEVC Low Boom Supersonic Inlet Design Inlet Scale Information*

<i>Model</i>	<i>Acap (sq. in.)</i>	<i>Daip (in.)</i>	<i>Actual Scale</i>	<i>Approx. Scale</i>
<i>Test Scale</i>	<i>1.5631</i>	<i>1.5361</i>	<i>0.0231</i>	<i>1/43</i>
<i>Ref. Scale</i>	<i>381.57</i>	<i>24.0</i>	<i>0.3692</i>	<i>1/3</i>
<i>Full Scale</i>	<i>2802.0</i>	<i>65.0</i>	<i>1.0</i>	<i>1/1</i>

# *Boeing QEVC Low Boom Supersonic Inlet Design 8x6 SWT Conditions for Test*

<i>Variable</i>	<i>Value</i>
<i>Tunnel Mach Number, <math>M_0</math></i>	<i>1.560</i>
<i>Tunnel Total Pressure (lbs/ft<sup>2</sup>), <math>P_o</math></i>	<i>2942.9</i>
<i>Tunnel Total Temperature (°R), <math>T_o</math></i>	<i>627.0</i>
<i>Reynolds Number, <math>Re_{Daip}</math></i>	<i><math>6.275 \times 10^5</math></i>

# *Boeing QEVC Low Boom Supersonic Inlet Design Response Variables*

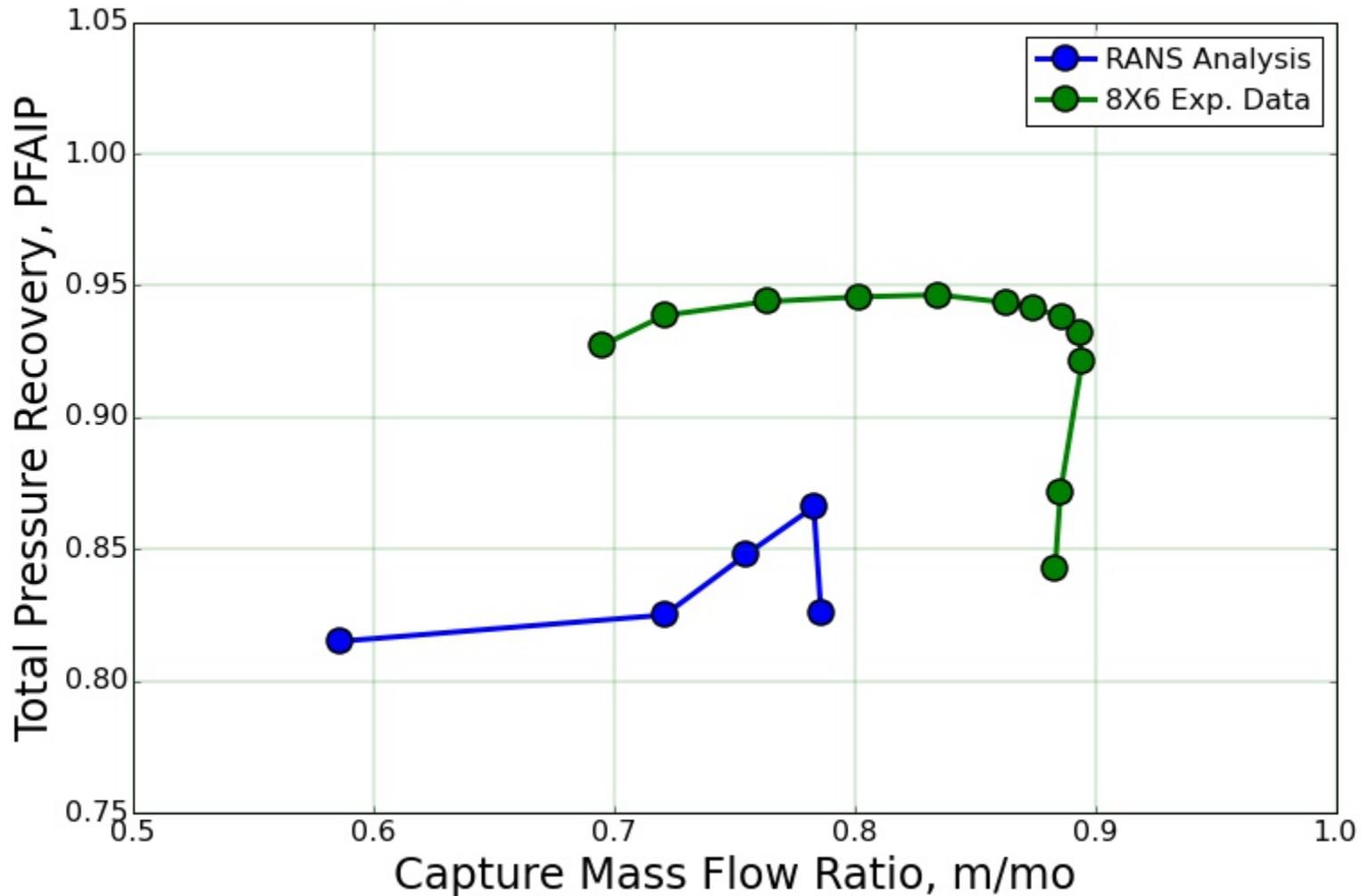
<i>Response Variable</i>	<i>Symbol</i>
<i>Area Averaged Capture Mass Flow</i>	<i><math>m/m_0</math></i>
<i>Area Averaged AIP Total Pressure Recovery</i>	<i>PFAIP</i>
<i>AIP Circumferential Distortion</i>	<i>DPC/P</i>

# *Boeing QEVC Low Boom Supersonic Inlet Design Time Relevant Variables*

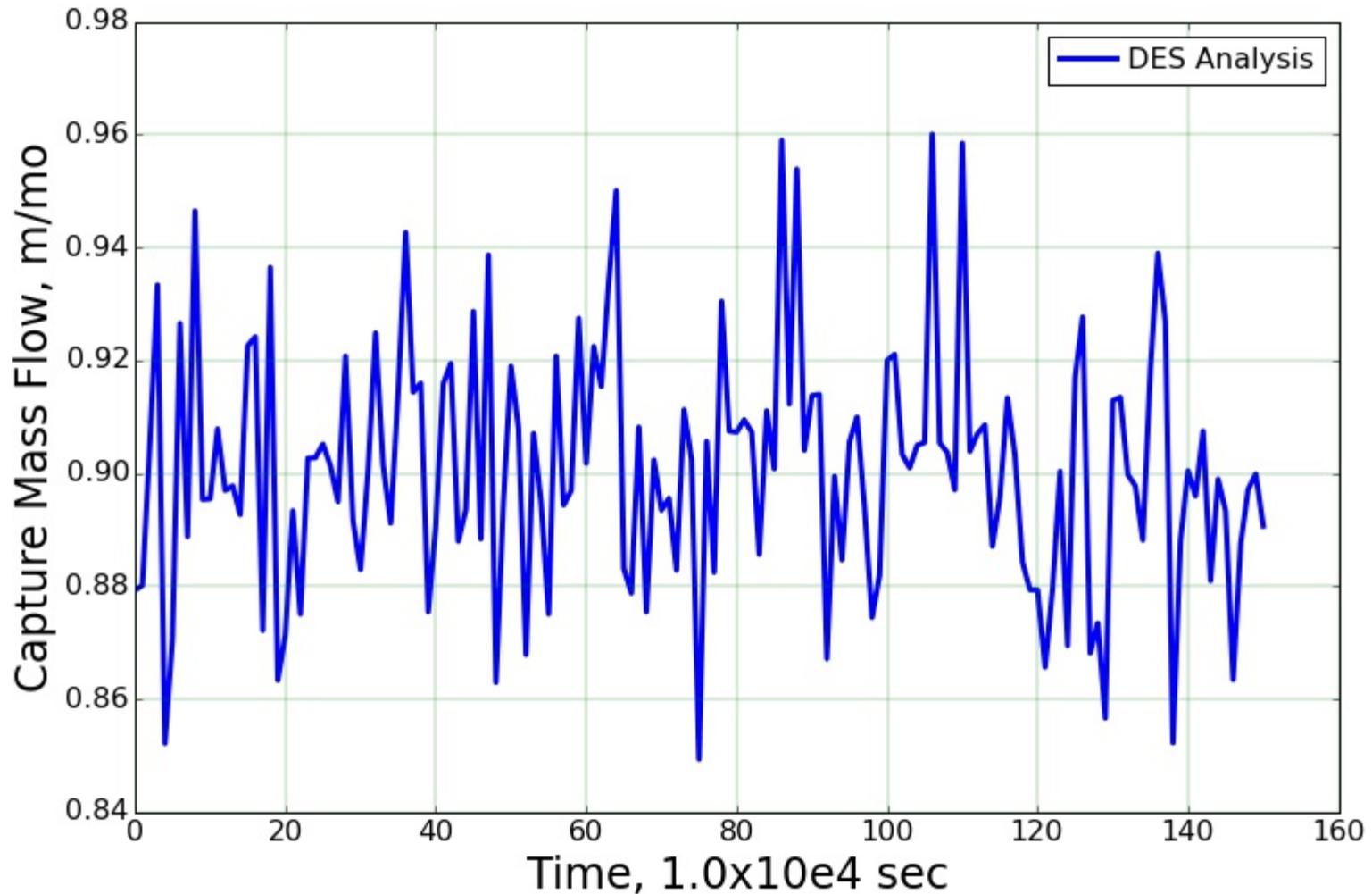
<i>Time Variable</i>	<i>Value</i>
<i>Computational Time Step, Sec.</i>	$5.0 \times 10^{-7}$
<i>CFD Data Sampling Rate, Sec</i>	$1.0 \times 10^{-4(1)}$
<i>Per/Rev Time Span (4300 RPM), Sec.</i>	$1.395 \times 10^{-2}$
<i>CFD Data Per/Rev Sampling Time Span, Sec <sup>(1)</sup></i>	$1.4 \times 10^{-2}$
<i>Total Number of Data Samples</i>	141

*(1) Equivalent to experimental sampling rate,  $1.0 \times 10^4$  samples/sec*

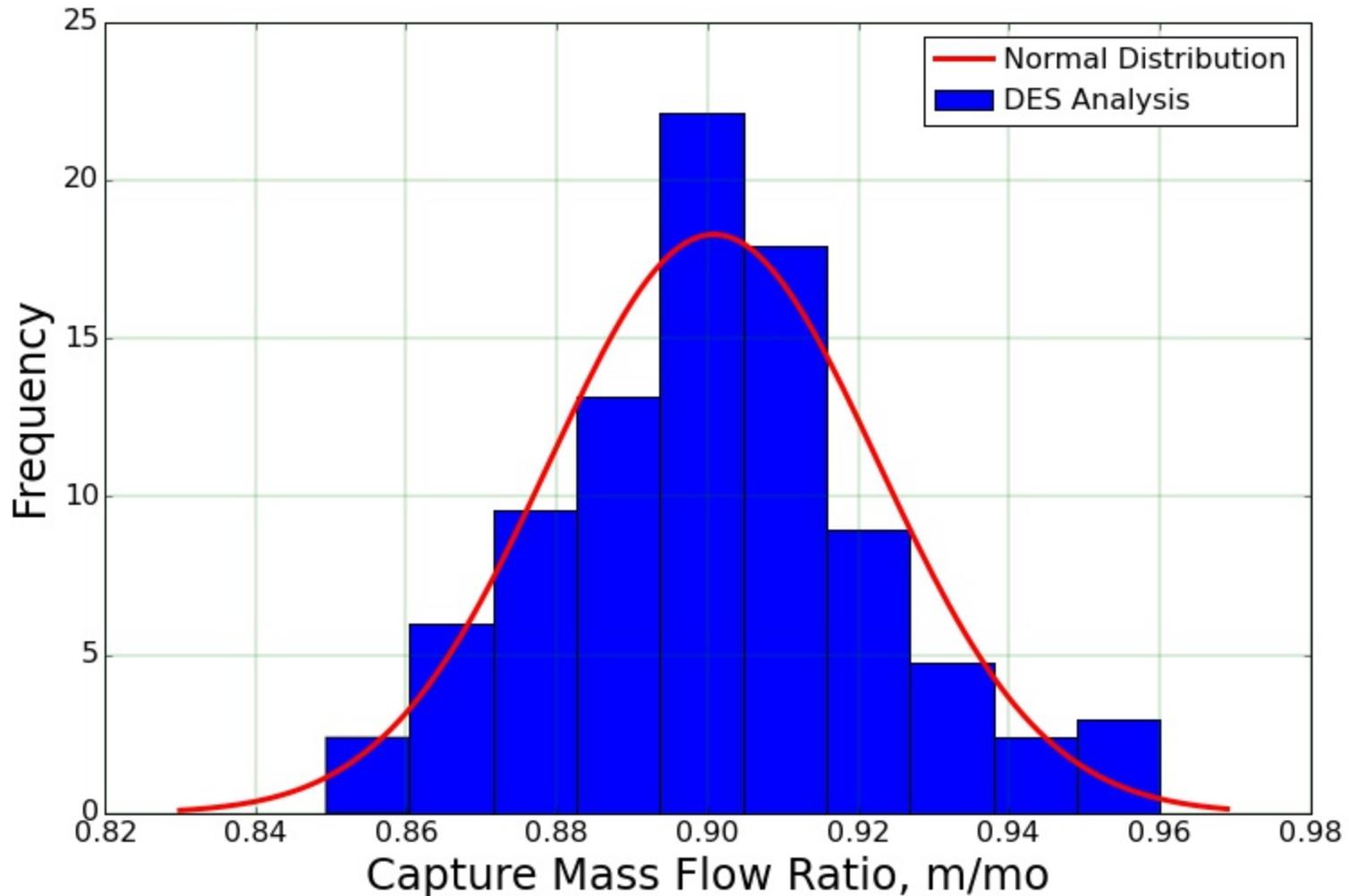
*Boeing QEVC Low Boom Supersonic Inlet Design*  
 *$Re = 6.275 \times 10^5$ , Scale  $\approx 1/43$ ,  $M_0 = 1.560$*   
*Steady PFAIP Cane Curve*



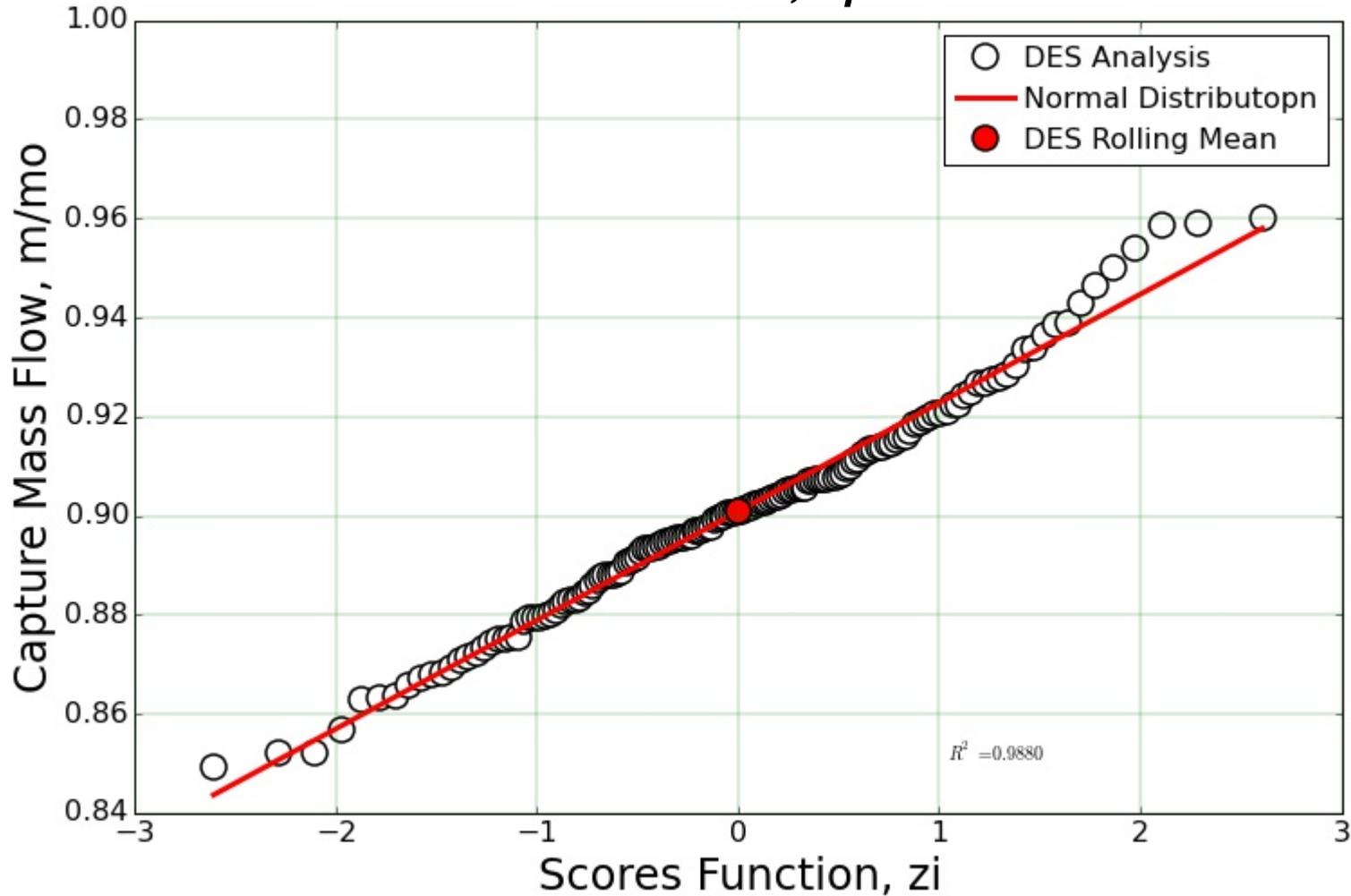
*Boeing QEVC Low Boom Supersonic Inlet Design  
Critical Operating Condition,  $M_0 = 1.560$   
Capture Mass Flow Ratio,  $m/m_0$*



*Capture Mass Flow  $m/m_0$  Probability Distribution  
Critical Operating Condition,  $M_0 = 1.560$   
 $m/m_0$  Histogram Plot*



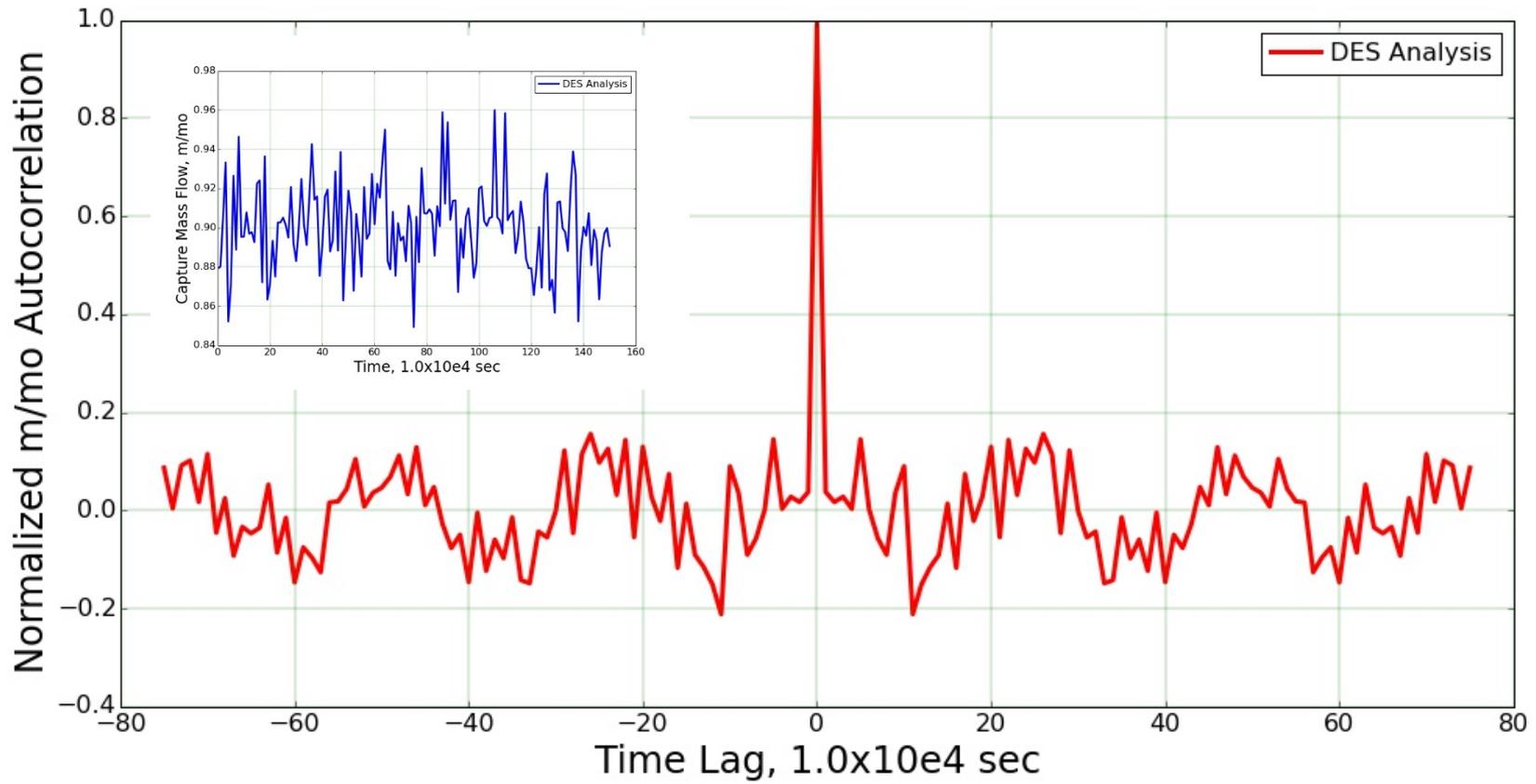
*Capture Mass Flow  $m/m_0$  Probability Distribution*  
*Critical Operating Condition,  $M_0 = 1.560$*   
*Normal Scores Plot,  $\rho = 0.9880$*



# Boeing QEVC Low Boom Supersonic Inlet Design

## Critical Operating Condition, $M_0 = 1.560$

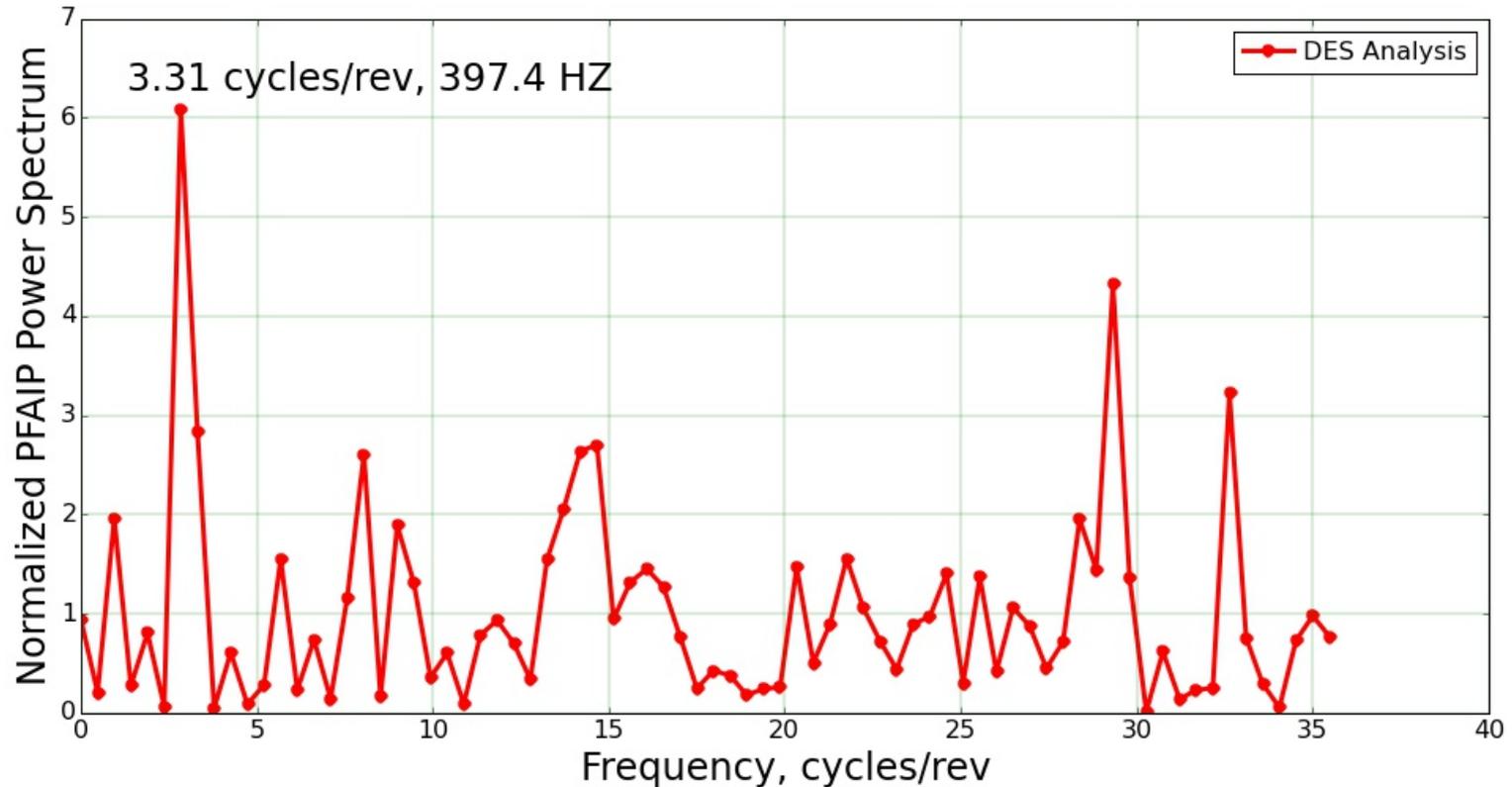
### Normalized $m/m_0$ Autocorrelation



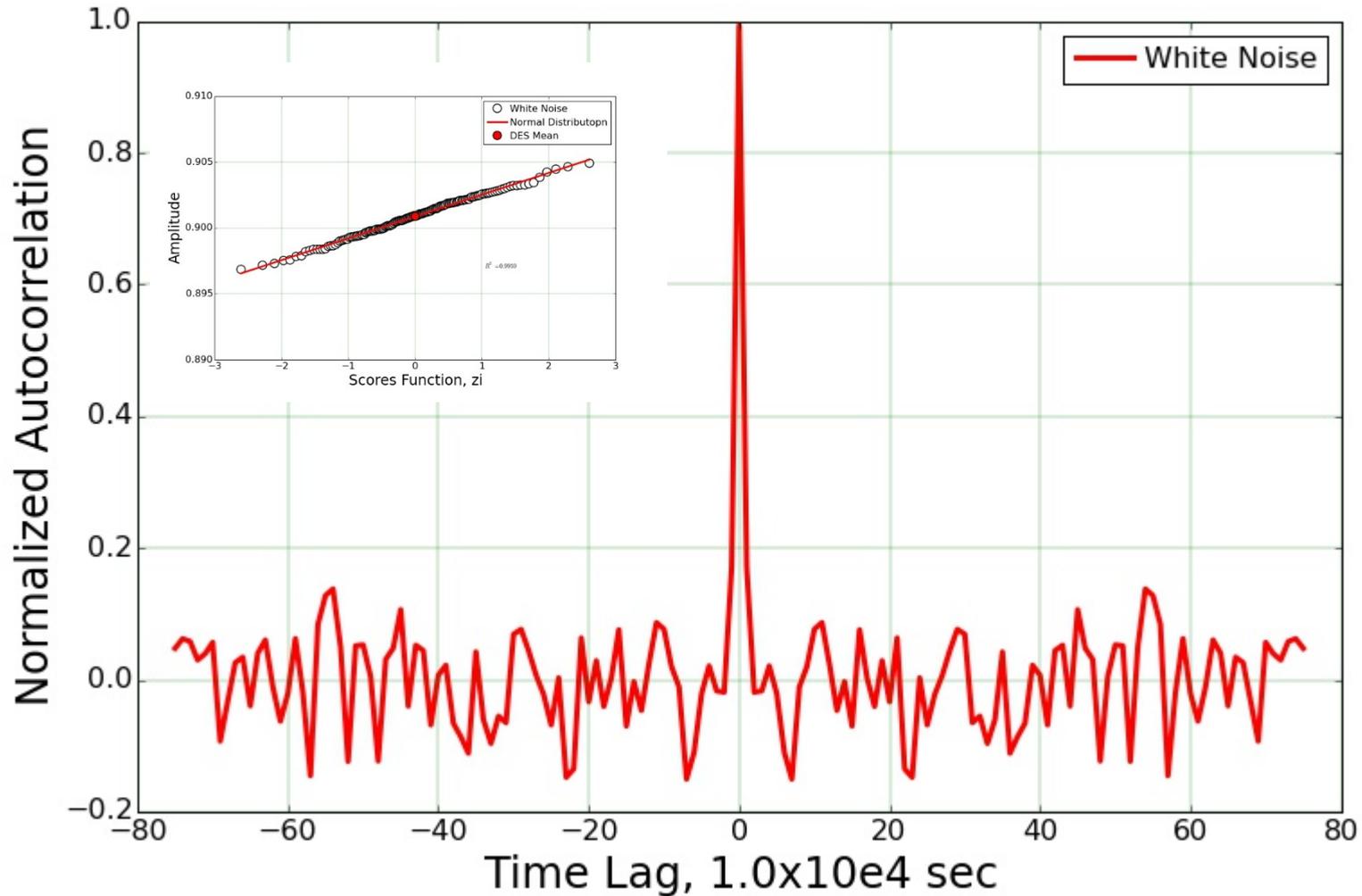
# Boeing QEVC Low Boom Supersonic Inlet Design

## Critical Operating Condition, $M_0 = 1.560$

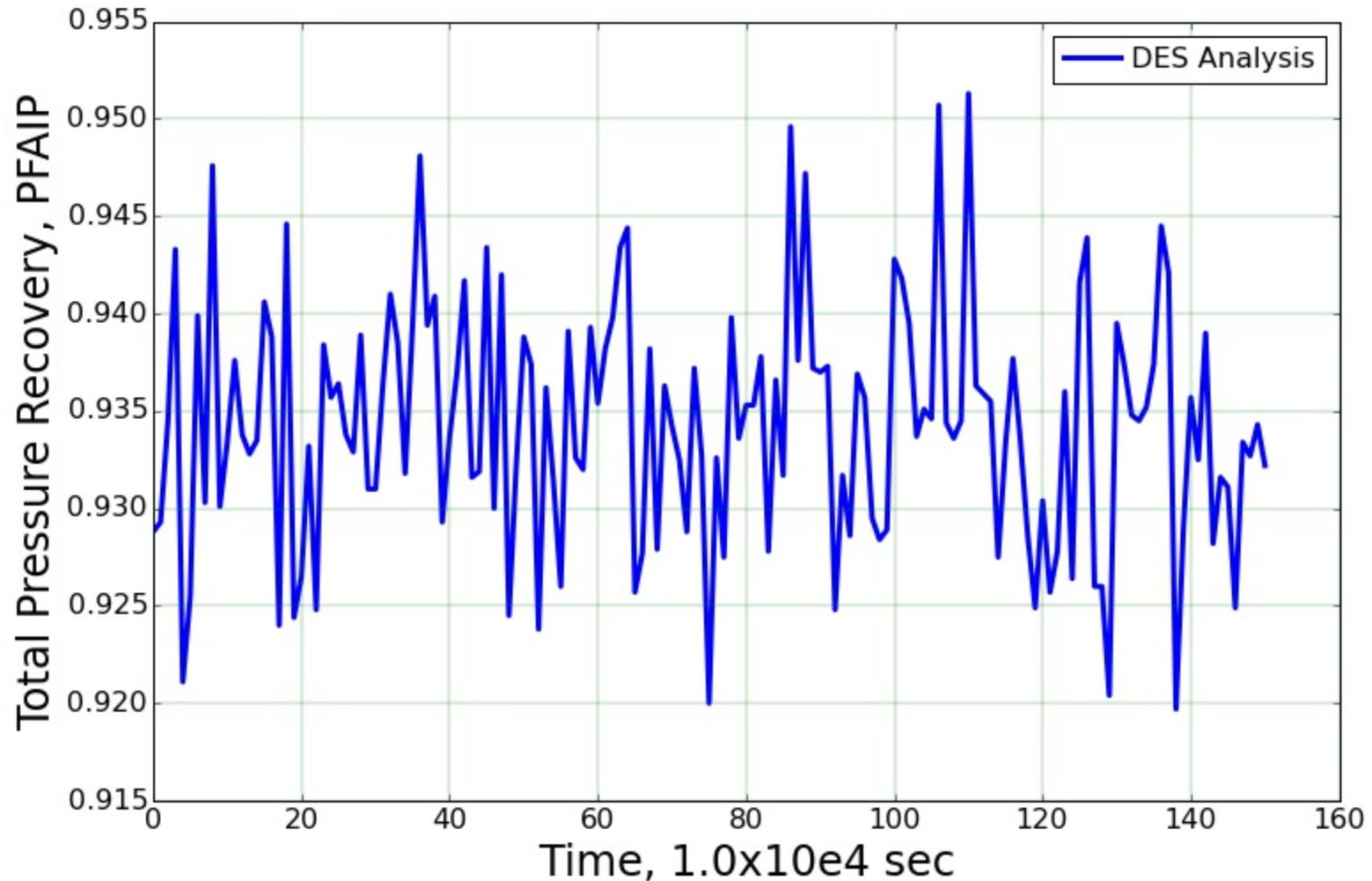
### Normalized $m/m_0$ Power Spectrum



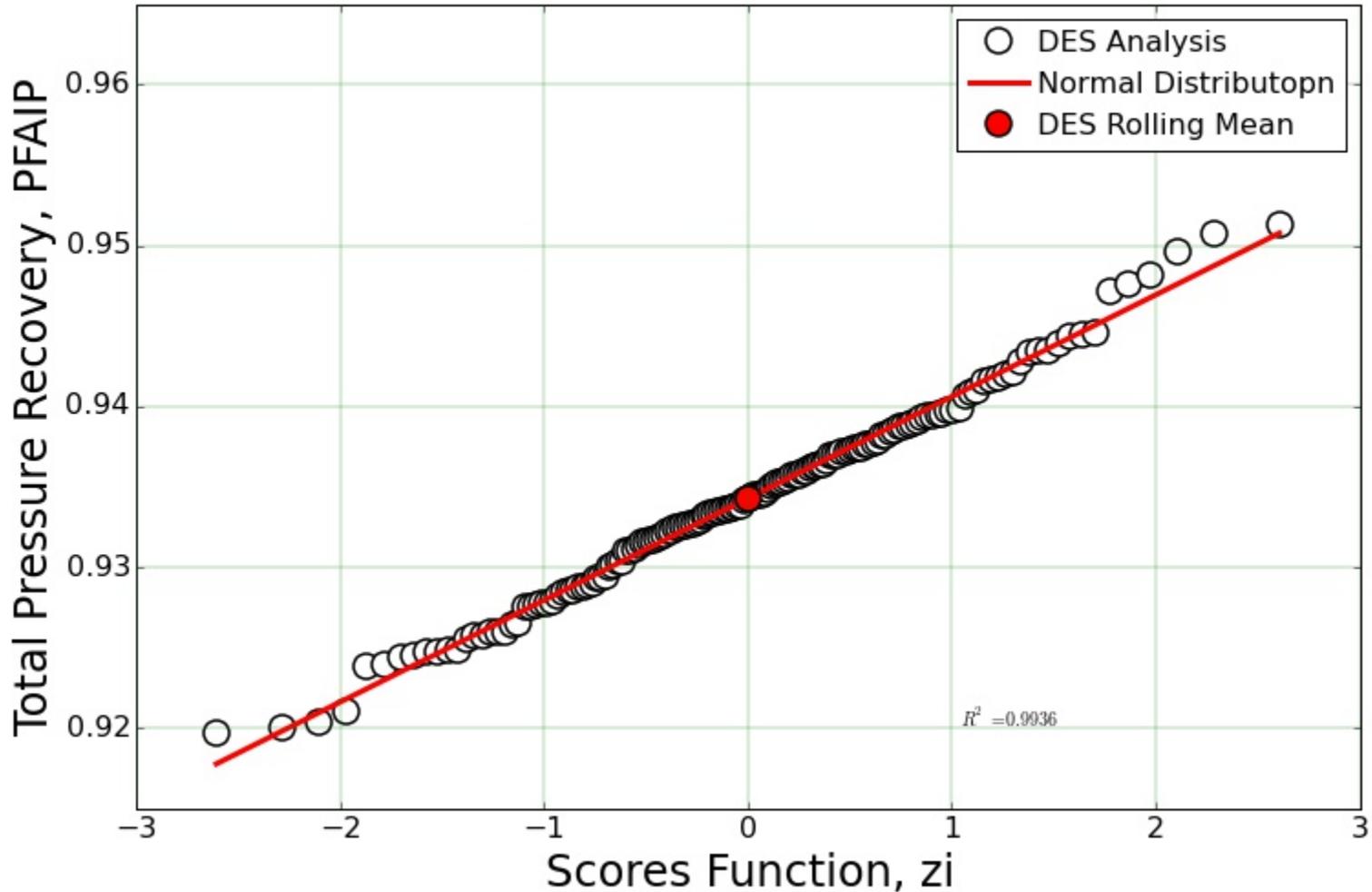
# Boeing QEVC Low Boom Supersonic Inlet Design Normalized Autocorrelation White Noise



*Boeing QEVC Low Boom Supersonic Inlet Design  
Critical Operating Condition,  $M_0 = 1.560$   
Total Pressure Recovery, PFAIP*



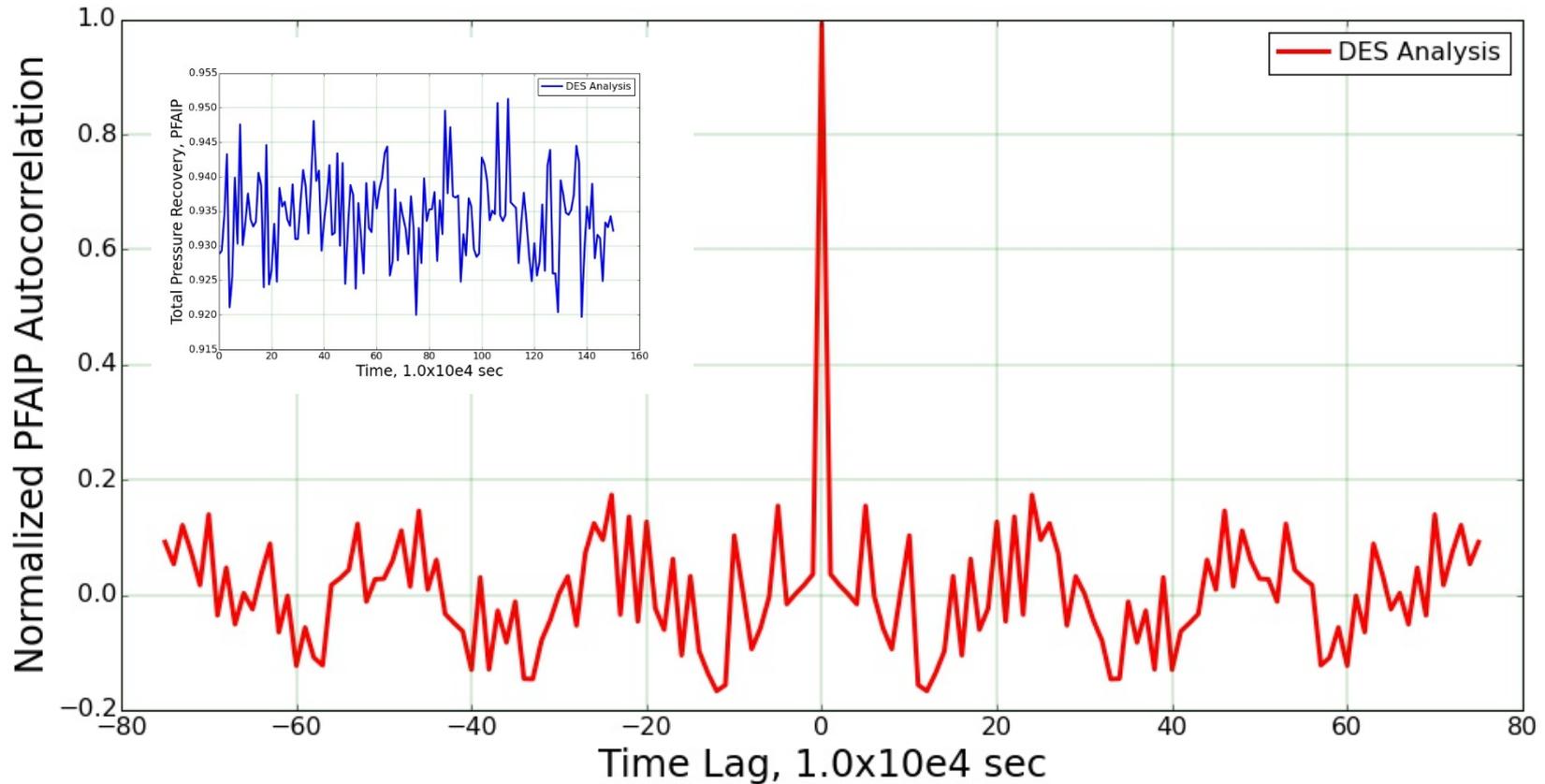
*Total Pressure Recovery PFAIP Probability Distribution  
Critical Operating Condition,  $M_0 = 1.560$   
Normal Scores Plot,  $\rho = 0.9906$*



# Boeing QEVC Low Boom Supersonic Inlet Design

## Critical Operating Condition, $M_0 = 1.560$

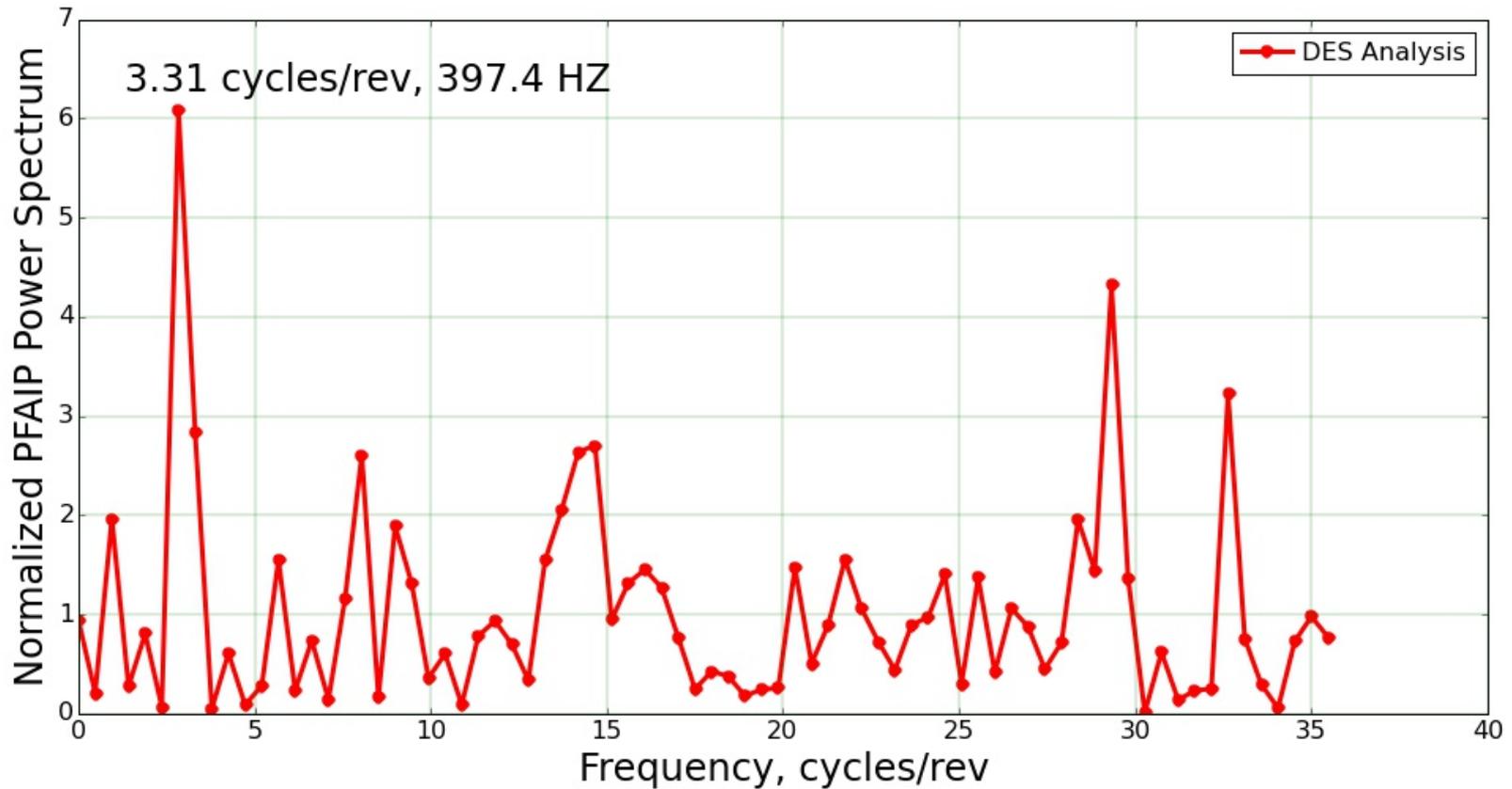
### Normalized PFAIP Autocorrelation



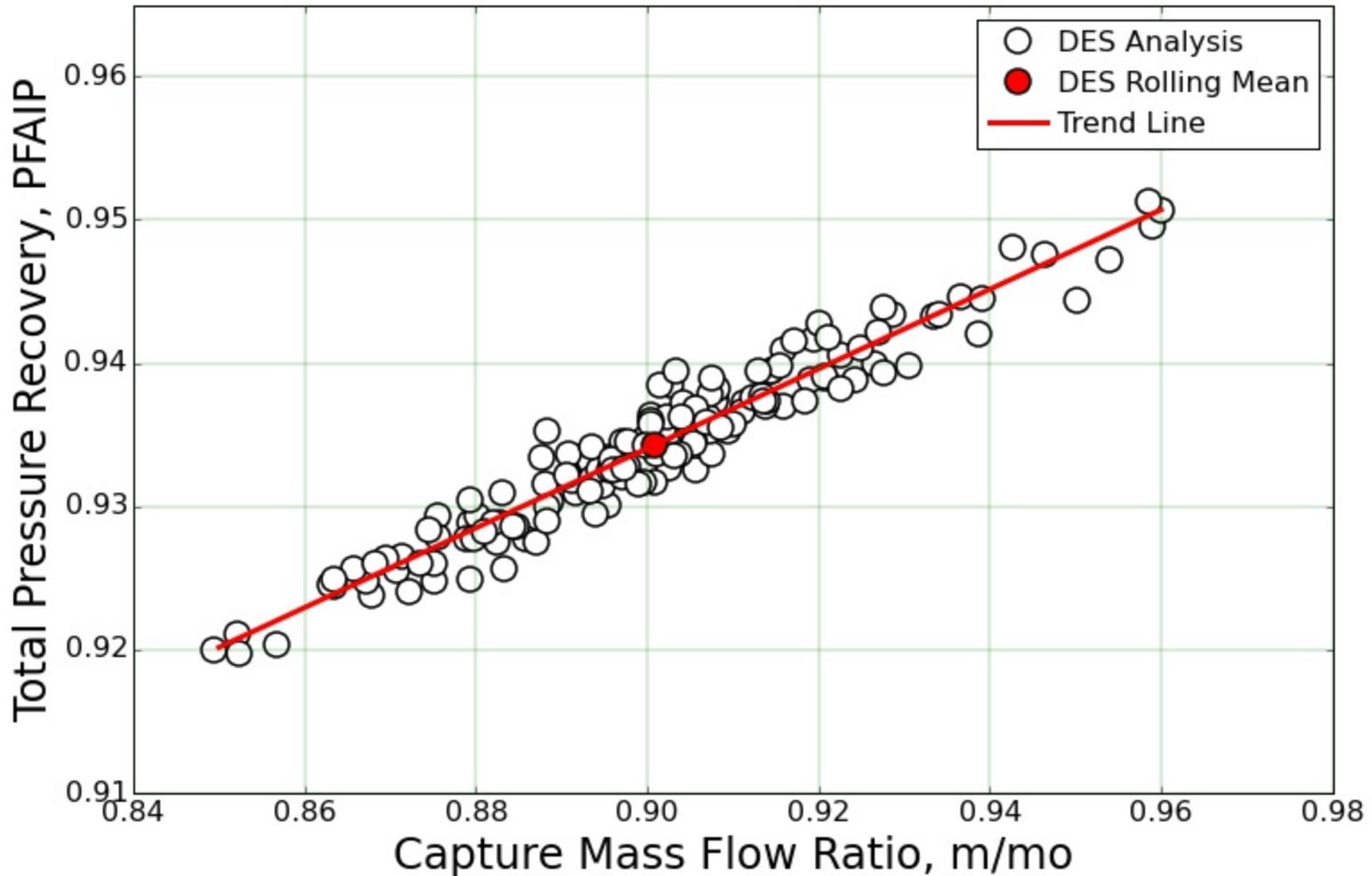
# Boeing QEVC Low Boom Supersonic Inlet Design

## Critical Operating Condition, $M_0 = 1.560$

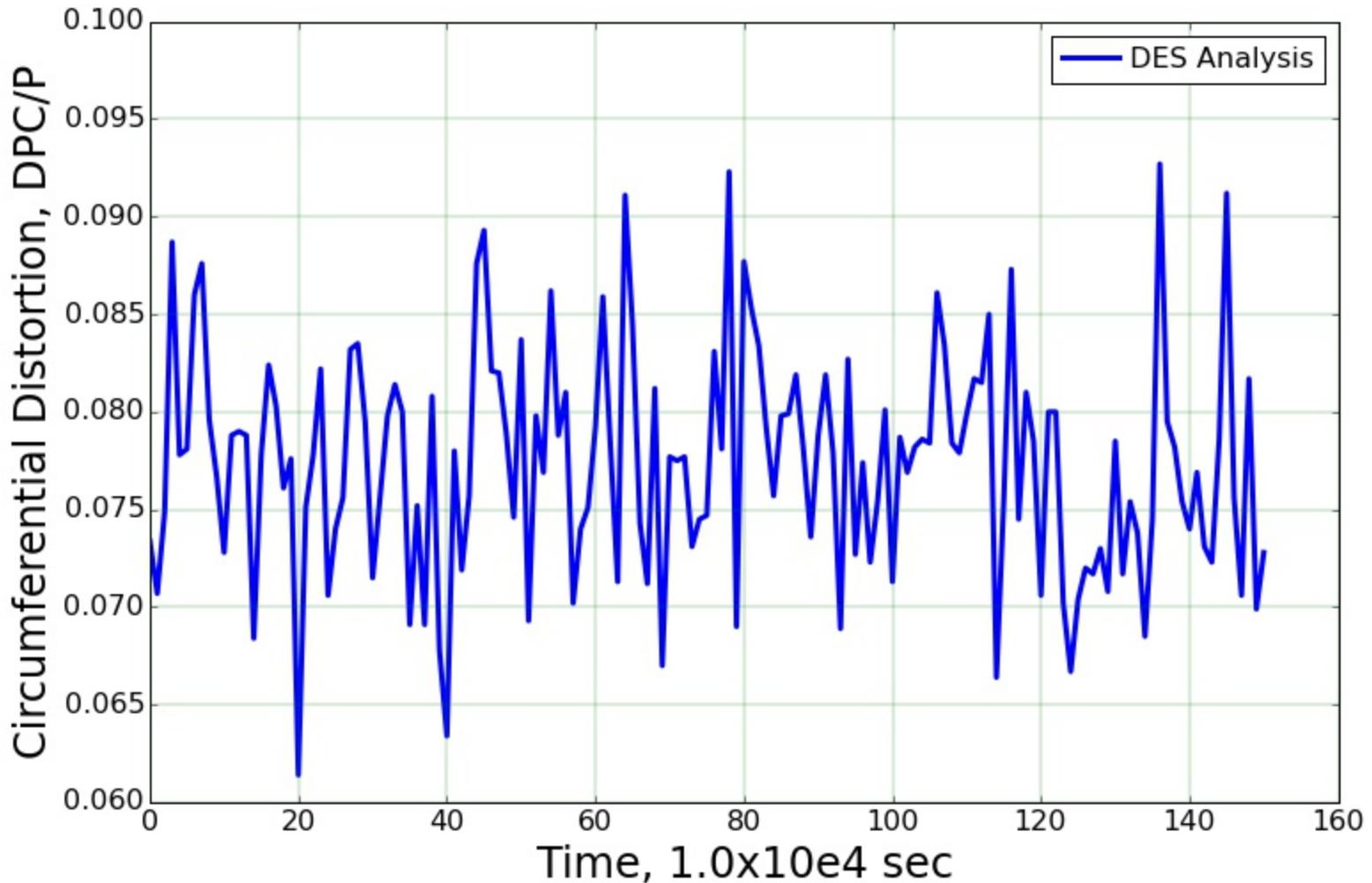
### Normalized PFAIP Power Spectrum



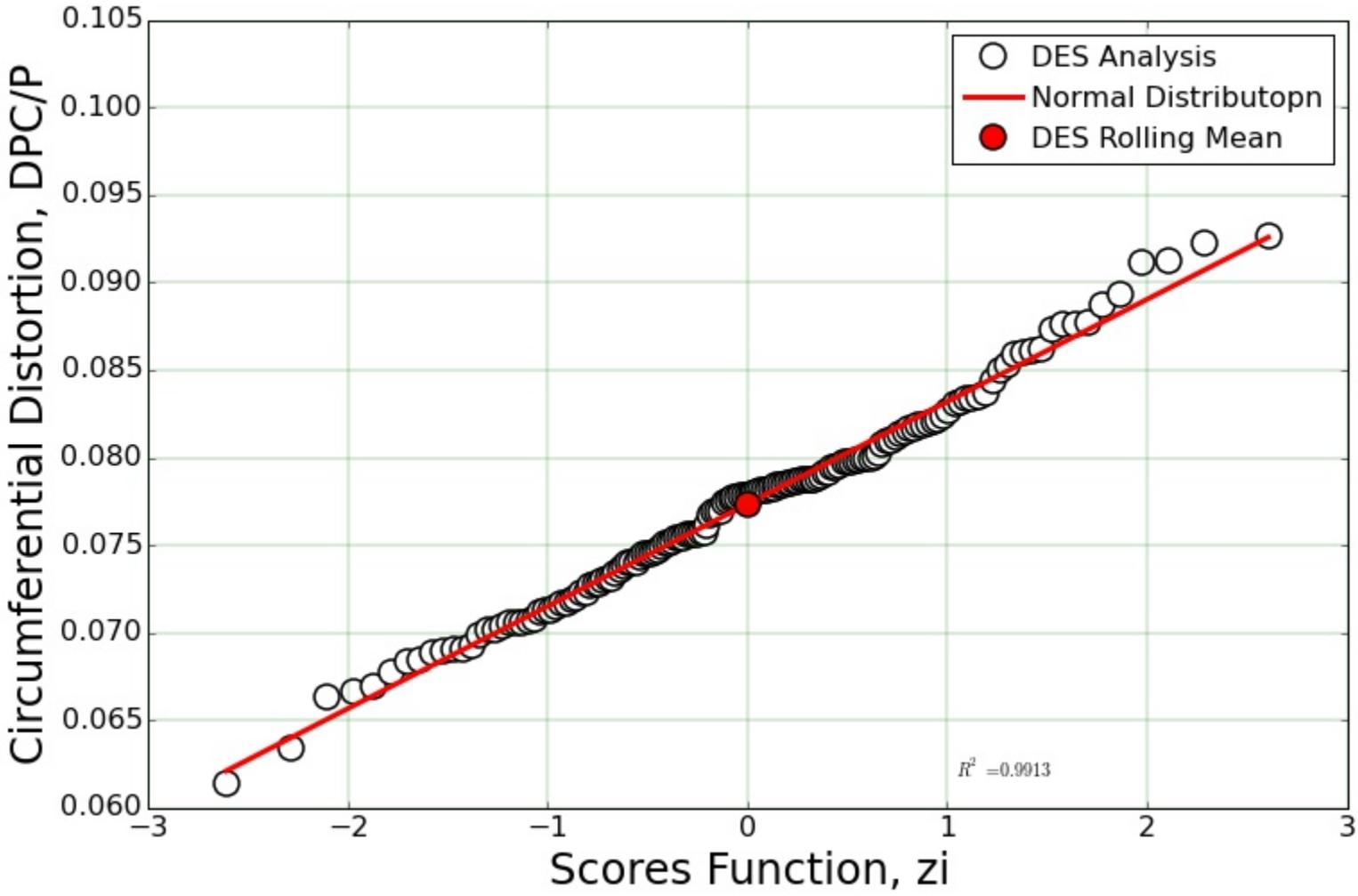
*Boeing QEVC Low Boom Supersonic Inlet Design  
Critical Inlet Operation,  $M_0 = 1.560$   
Scatter Plot,  $\rho = 0.984$*



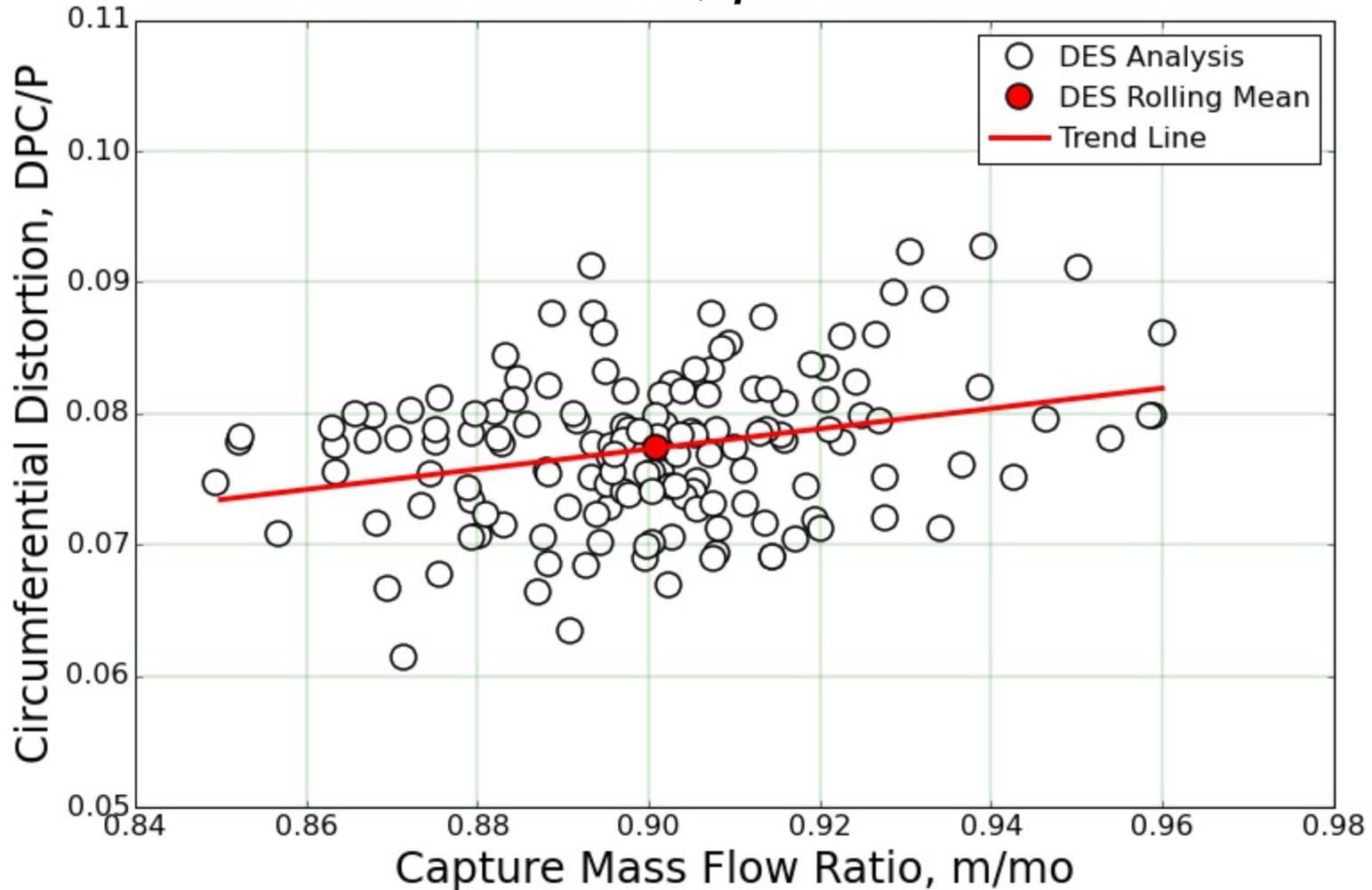
*Boeing QEVC Low Boom Supersonic Inlet Design  
Critical Operating Condition,  $M_0 = 1.560$   
Total Pressure Recovery,  $DPC/P$*



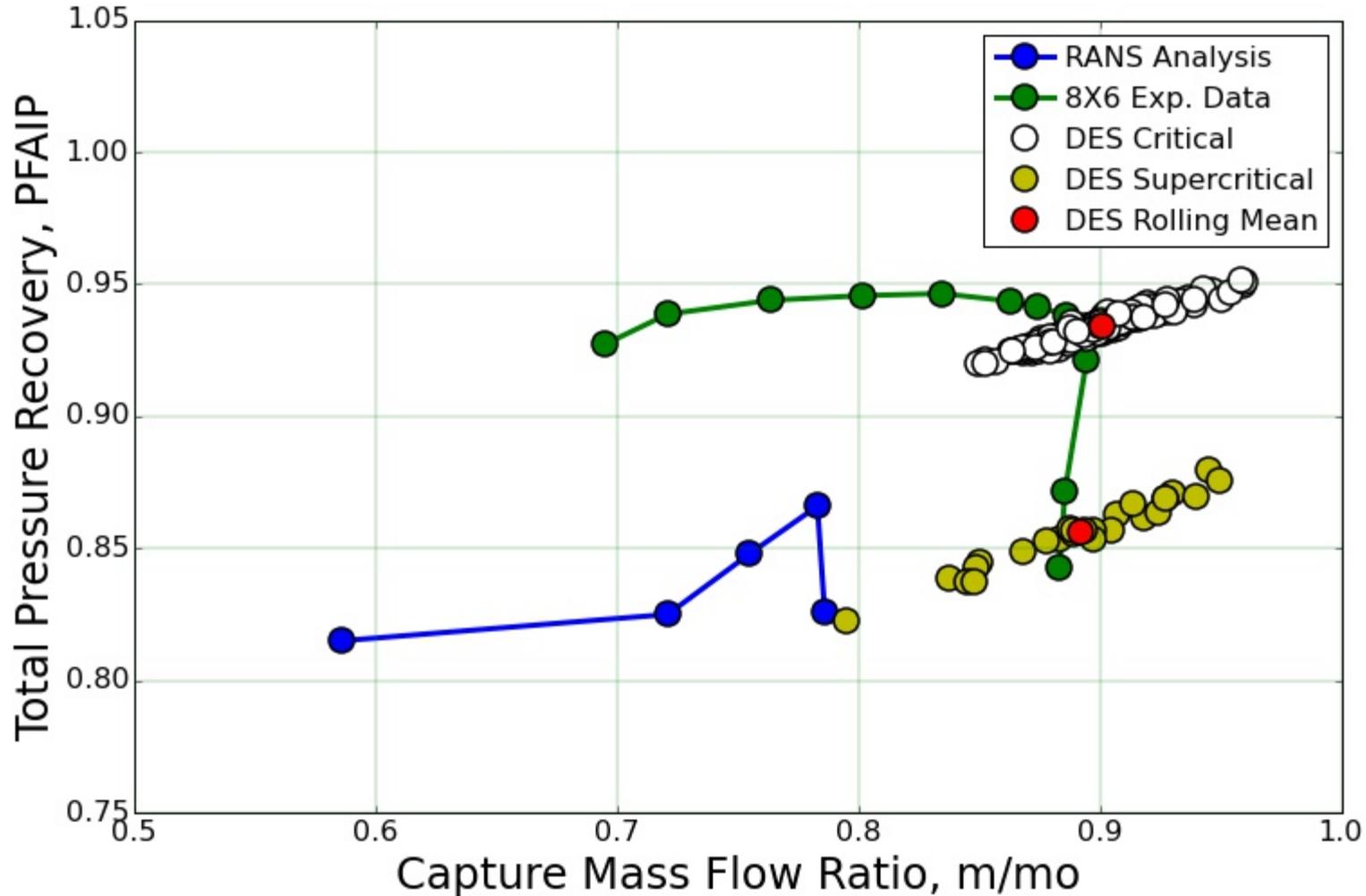
*Circumferential Distortion DPC/P Probability Distribution  
Critical Operating Condition,  $M_0 = 1.560$   
Normal Scores Plot,  $\rho = 0.9913$*



*Boeing QEVC Low Boom Supersonic Inlet Design  
Critical Inlet Operation,  $M_0 = 1.560$   
Scatter Plot,  $\rho = 0.289$*

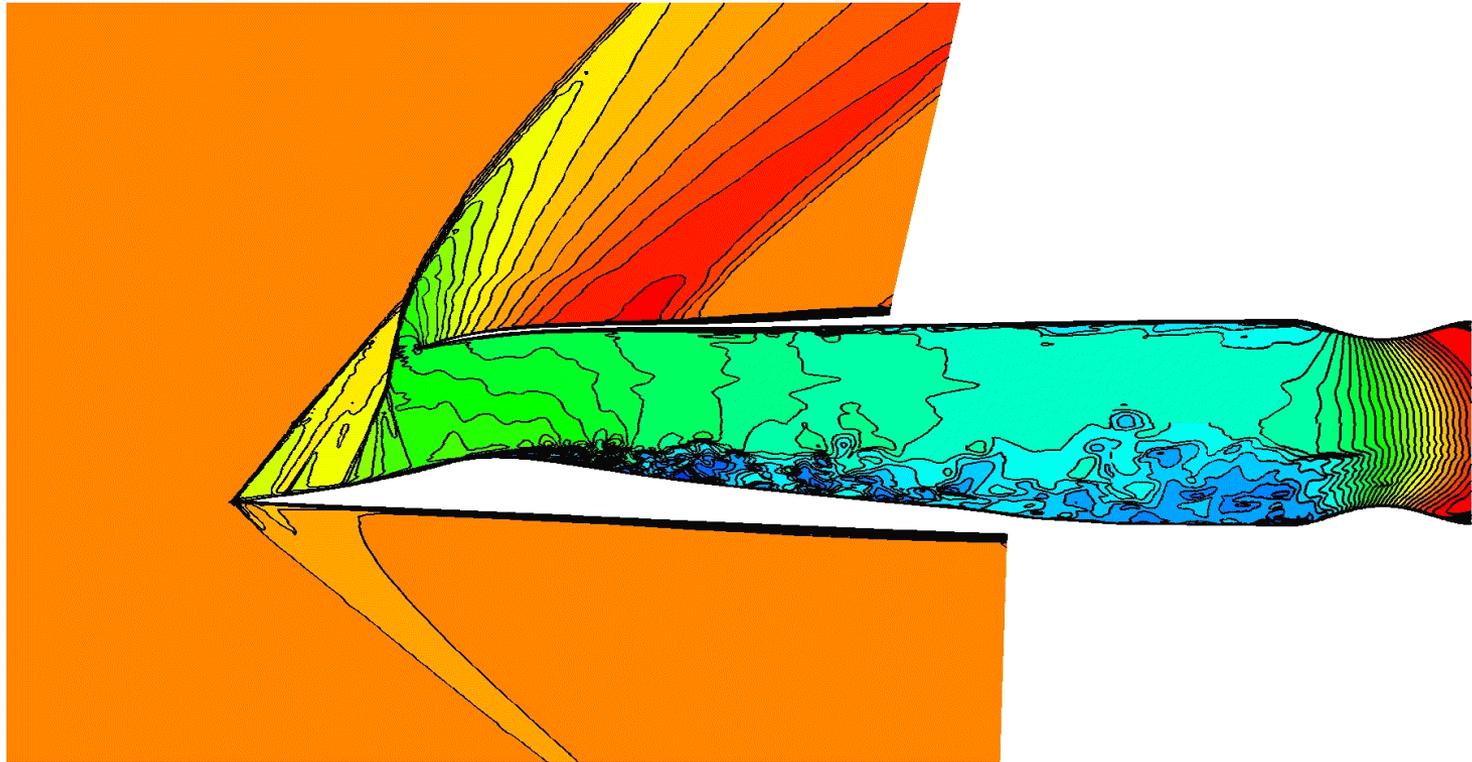


*Boeing QEVC Low Boom Supersonic Inlet Design*  
 *$Re = 6.275 \times 10^5$ , Scale  $\approx 1/43$ ,  $M_0 = 1.560$*   
*Unsteady PFAIP Cane Curve*

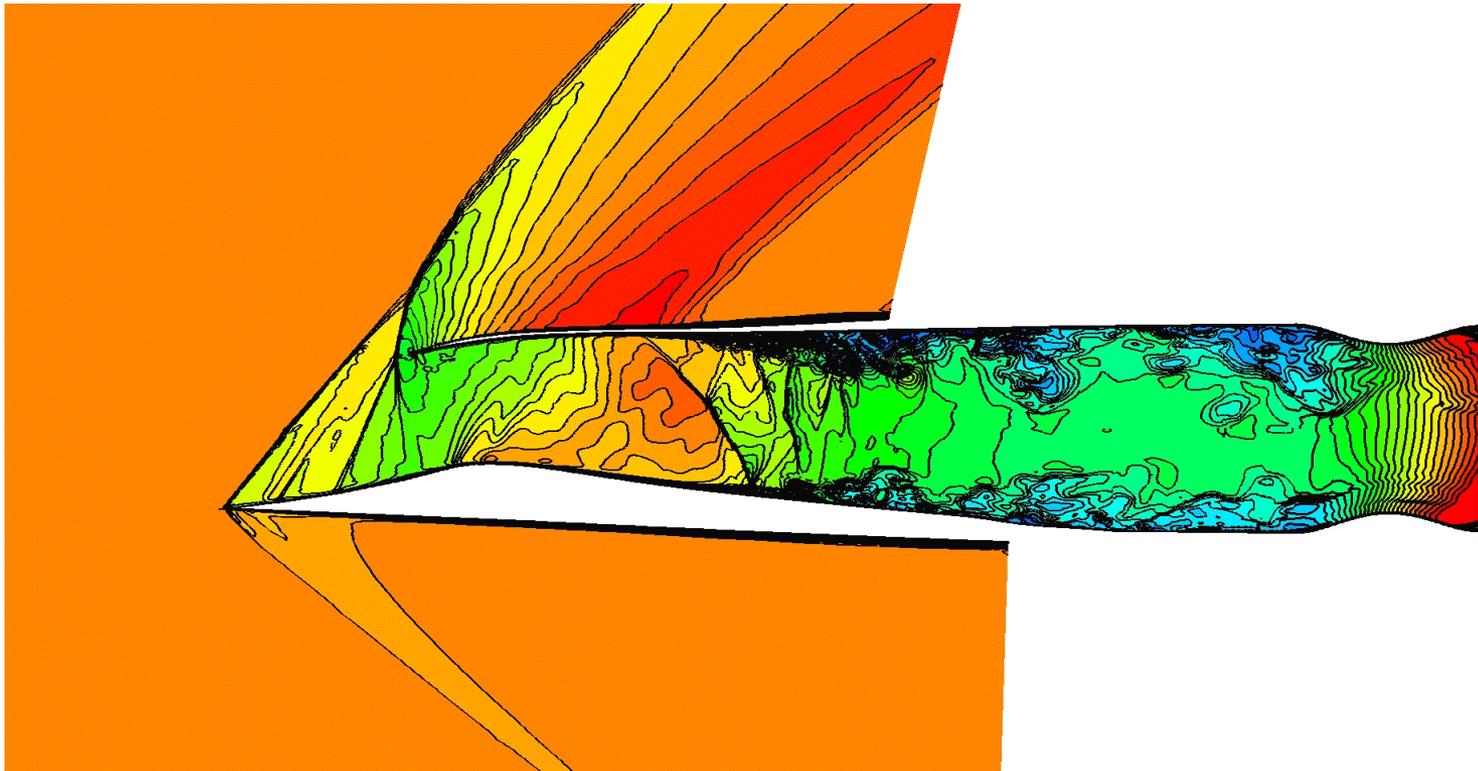




*Boeing QEVC Low Boom Supersonic Inlet Design  
Critical Inlet Operating Condition,  $M_0 = 1.560$   
Streamwise Mach Number Contours*



*Boeing QEVC Low Boom Supersonic Inlet Design  
Supercritical Operating Condition,  $M_0 = 1.560$   
Streamwise Mach Number Contours*



# *Statistical Nature of Unsteady Inlet Flow*

## *General Conclusions*

- 1. DES solutions to unsteady inlet flows can give very good results, however, they are very costly, time consuming to analyze, and have many caveats associated the CFD analysis.*
- 2. The unsteady flow associated with the QEVC Low Boom Supersonic Inlet Design was non-stationary, i.e. it has a mean flow that varies with time (commonly called a “rolling mean”) at 3.31 cycles/rev or 397.4 HZ.*
- 3. In spite of the fact that the unsteady flow exhibited a near perfect normal probability distribution, there existed a coherent structure in the time series.*
- 4. There is a high correlation ( $\rho = 0.984$ ) between unsteady capture mass flow ratio ( $m/m_0$ ) and unsteady total pressure recovery (PFAIP).*
- 5. There is a low correlation ( $\rho = 0.289$ ) between unsteady capture mass flow ratio ( $m/m_0$ ) and unsteady circumferential distortion (DPC/P).*
- 6. In order to provide sufficient data for a complete time series analysis, data samples should cover a least four revolutions of the fan.*

# *Statistical Nature of Unsteady Inlet Flows*

## *Aerodynamic References*

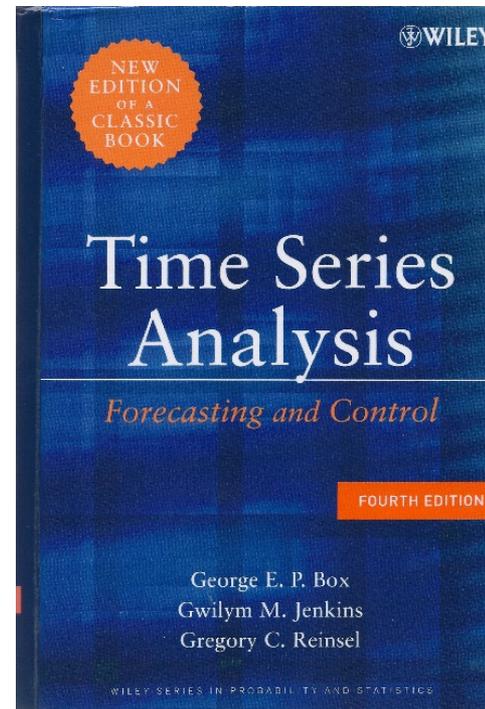
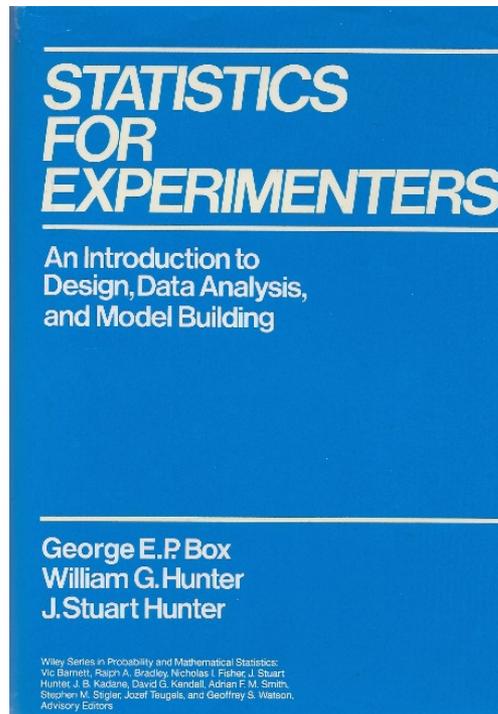
1. *Trefny, C J., Hirt, S. M., Anderson, B. H., Fink, L. E., and Magee, T. E., "Performance of a Supersonic Over-Wing Inlet with Application to a Low-Sonic-Boom Aircraft", AIAA Paper, 2014.*
2. *Mace, J, Lakebrink, M, Mani, M, and Steeken, W: "Computational Simulation of Dynamic Total Pressure Distortion, AIAA Paper, 2014.*

# Statistical Nature of Unsteady Inlet Flows

## Statistical References

3. Box, G. E. P., Hunter, W. G., and Hunter, J. S., “Statistics for Experimenters,” John Wiley, New York, 1978.

4. Box, E. P., Jenkins, G. M., and Reinsel, G. C.: “Time Series Analysis”, John Wiley & Sons, 2008.

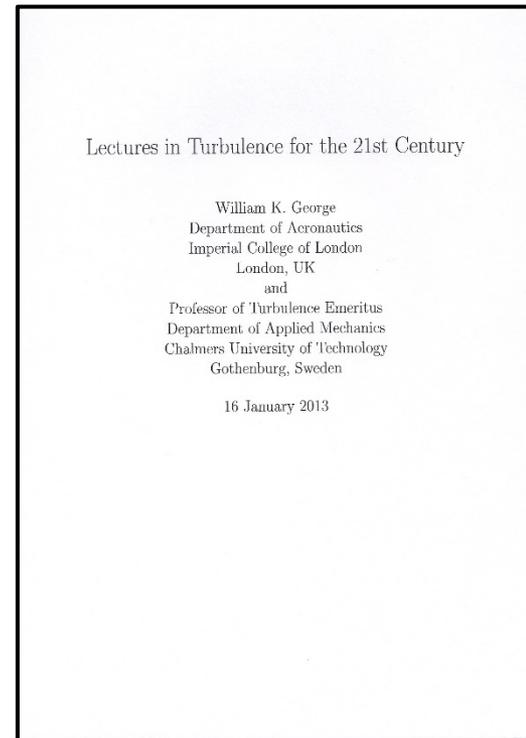


# *Statistical Nature of Unsteady Inlet Flows*

## *Turbulent Flow References*

5. Monin, A. S., and Yaglom, A. M., “*Statistical Fluid Mechanics*”, The MIT Press, Cambridge, Massachusetts, 1971

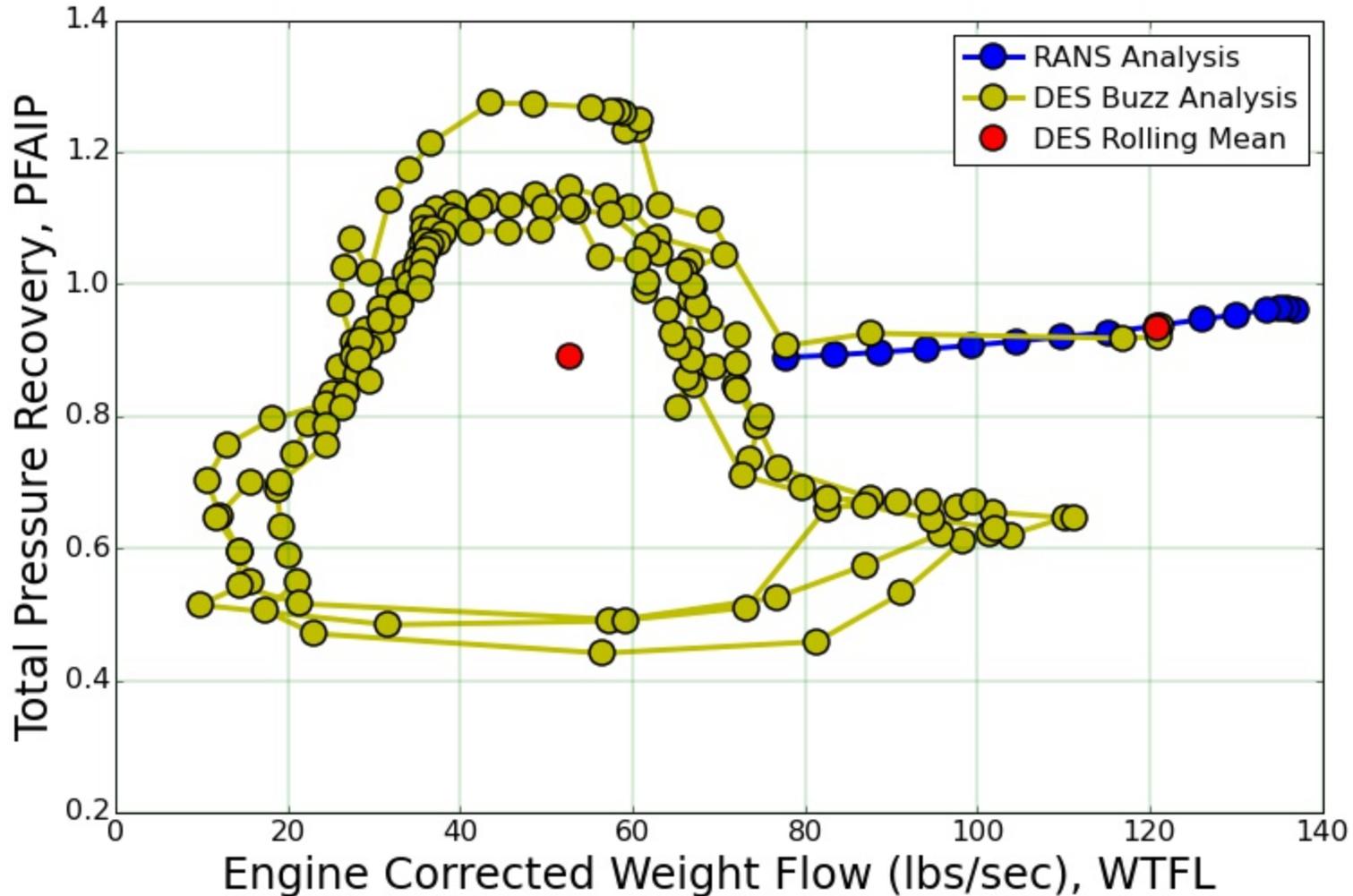
6. George, W. K.: “Lectures in Turbulence for the 21st Century”, January, 2013.



# *The Statistical Nature of Inlet Buzz*

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# LMCO Low Boom Supersonic Inlet Design Unsteady PFAIP Cane Curve, $M_0 = 1.70$ Analysis of Inlet Buzz

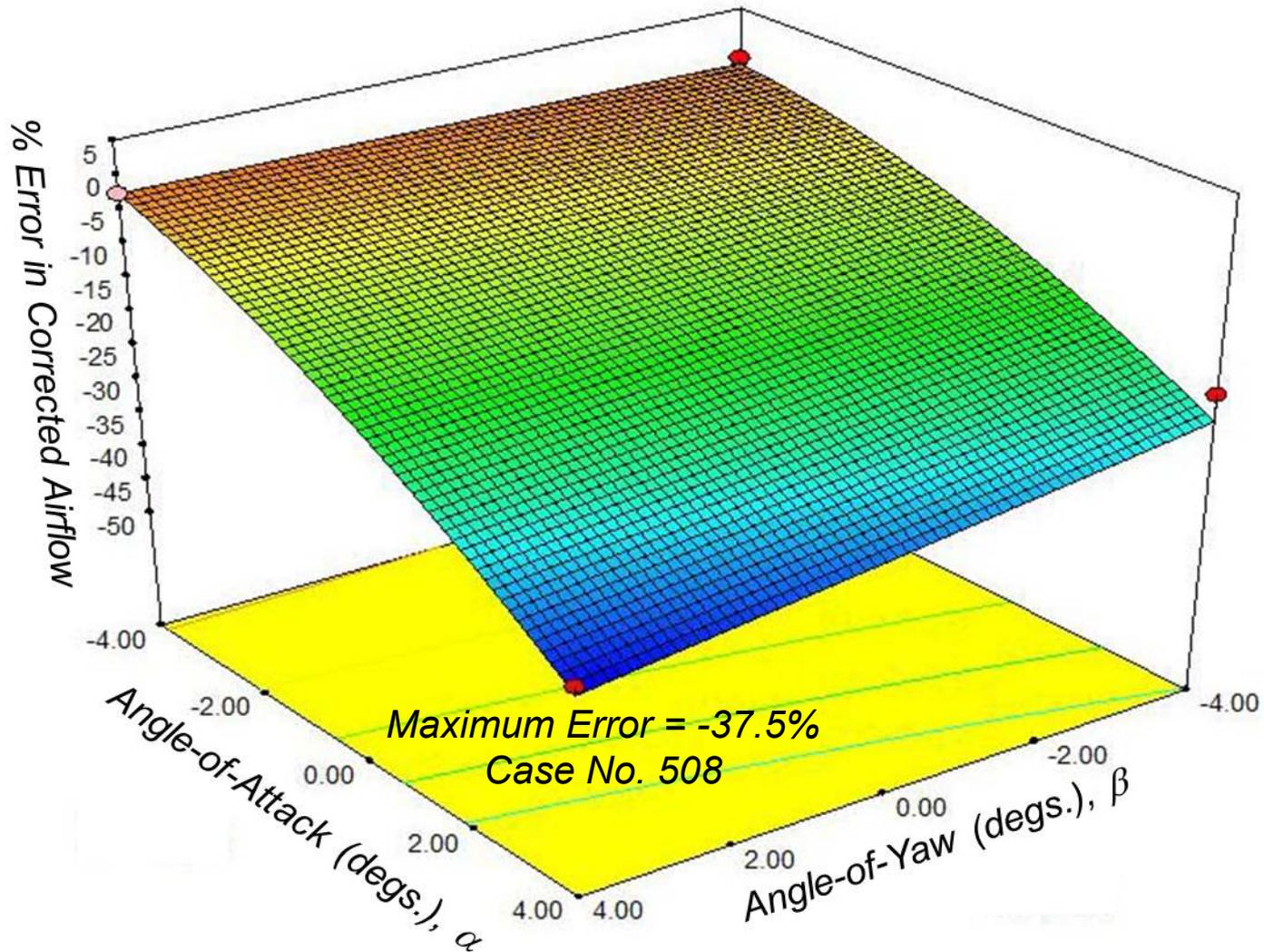


# *The Role of Design-of-Experiments Methodology in Unsteady Inlet Flows*

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# Boeing Low Boom Supersonic Inlet Design Engine Corrected Airflow Systemic Errors

$Re = 8.068 \times 10^6$ , Scale  $\approx 1/3$ ,  $M_0 = 1.80$



# *The Role of Autocorrelations in Turbulent Flow Studies*

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# Auto-Correlations in Turbulent Flow Taylor Micro-Scale Region

